Summary of Monitoring and Evaluation of In-Stream Works at Sites 14 and 15 in the Kitwanga River South Sub-Basin to March, 1999

Prepared for the Gitsegukla Band Council

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### Introduction

BioLith Scientific Consultants Inc. and Hydroglyphic Terrain Analysts were contracted by the Gitsegukla Band Council to prepare a summary of Monitoring and Evaluation of In-Stream Works as per Schedule A of the Standards Agreement with the Ministry of Environment. The following summary is based on first hand information derived from BioLith's and Hydroglyphics' involvement and on other information provided by the Band.

As a result of a Level I Overview Assessment of the Kitsegukla River watershed (Wild Stone 1995) and subsequent Level I Detailed Field Assessments of the South Sub-Basins of each system (Giesbrecht and Grieve 1998), restorative works in and around the streams were prescribed for a number of sites, including Prescription Sites 14 and 15 in the Kitwanga River South Sub-Basin (see Figure 1).

This report summarizes the monitoring program to assess the effectiveness of the restoration activities. The report includes results of the data gathered to begin the process of monitoring changes that result from the restorative treatments, and provides details of the overall monitoring plan recommended for gathering more data. When more data is gathered in the future, it will be possible to compare that data with the data gathered to date to assess the effectiveness of the treatments applied, to make necessary changes to the restorative works and to beneficially influence plans for other treatments in the future.





### **Monitoring Plan**

# Biological Monitoring - G. Grieve, R.P. Bio.

The efficacy of the restorative treatments implemented can only be assessed through quantitative comparisons of parameters measured before and then after construction (see also Gilchrist 1998). The two most significant parameters to measure are changes to fish populations and changes to fish habitat. Only limited data on each of these characteristics is available from the Level I assessment, as that process involved sampling of representative parts of a much larger portion of the watershed. A reasonably valid assessment of efficacy will require a more intensive program of measurements. In particular, the construction site should be the subject of an intensive topographic survey of the stream's channel to determine its characteristics over time, along with an intensive fishing program to determine changes in the fish population over time.

### Fish Habitat

The physical characteristics of samples of the stream (Giesbrecht et al, 1998), and the pre-construction survey provide some 'before' data. The as-built survey data for all of Site 14 and for the mid-channel bar portion of the lower channel of Site 15, however, are not relevant as 'before' data because these channels were altered significantly during construction.

It is recommended that the stream channels should be the subject of an intensive topographic survey, using a total station, to quantify the shape of the channels before the spring freshet produces the first significant alterations. The same procedure should then be repeated at least once each year for five years and for a minimum of three '1 in 25 year' flood events.

This survey will require x, y and z coordinate information in a grid pattern at a minimum resolution of one datum/m. The survey should extend from the culverts at each site to the mouth and should extend at least 5 horizontal metres 'inland' from the bankfull edge. In the areas immediately adjacent to the installed functional structures, a greater resolution is required to detect significant change. This information should be plotted in the form of a contour map at a scale of at least 1:200 with a contour interval of at least 0.1 m. A total station allows the rapid repeat of these measurements at the same points in future years. This map should then be compared with maps generated using the same methods in future years. It will be necessary to quantify the measurement of change using these maps. This could be done using a random sampling technique and by exploiting the analytical power of 3D software such as a GIS or CAD package. For example, using this technology and the data described above, it would be possible to define an habitat characteristic such as deep pool habitat by establishing numeric criteria and then having the software measure the quantity objectively.

In addition to the survey of the channel topography, the locations and orientations of the LWD structures should also be measured again with a total station. This should begin after the spring freshet during low water in late summer. The same procedure should then be repeated at least once each year for five years and for a minimum of three '1 in 25 year'

flood events. If any of the LWD moves, then its fate should be followed by finding it and its identity (each piece was tagged with an aluminum tag placed so that it would not likely come off during movement) so that its history could be reconstructed.

The Fish Habitat Assessment Procedure (FHAP) should be applied to these sites to measure before and after conditions with the same frequency and duration as described above. The FHAP data can also be compared with similar data gathered during the original FHAP done at representative sites within these or other tributaries.

A photographic record of the sites should also be compiled over time using the photo points that were established during construction.

The streams should be walked at least once each year after the spring freshet in order to determine what maintenance or improvements are required.

#### Fish

Fish data too is limited to that provided by sampling of these and similar streams during the Level I field assessment (Giesbrecht et al, 1998). The sites should be fished intensively to determine species composition, micro-distribution, and relative abundance. Relative abundance could best be determined through a mark-recapture program at each site. This work should be done before the spring freshet to get as much 'before' data as is possible.

Most fishing programs involve intensive fishing once a year. Given that fish are migratory to some degree during all free swimming phases of their life cycle, the fishing program should involve fishing at least three times throughout the year. It is recommended that the site be fished intensively each year for at least four years, as soon after winter as the crew can get to the site and the stream is open, again during high but not peak flows (especially sampling any off channel habitat) and again during late summer low flow conditions when the water temperature is between 8°C and 15°C. Similarly intense repetitions of the methods used should be implemented each year, beginning after the spring freshet in 1999, and continuing for at least four years, in order to produce reasonably valid assessments of the efficacy of the treatments.

The preferred fishing method involves roe baited minnow (Gee) traps set for a maximum of two hours in all habitat types. Such short sets reduce the effects of escape and predation that may bias the results of overnight sets and are more cost effective in that a site does not have to be visited on successive days. It is further recommended that the mark and recapture method of population size estimates include these short sets with no more than one week between the mark and the recapture efforts. No stop nets should be used.

### Geomorphological Monitoring - Dr. A. Gilchrist

The monitoring and evaluation of aquatic habitat rehabilitation requires the periodic measurement of both biological and physical factors. This section deals with monitoring the physical characteristics, or geomorphology, of streams that are affected primarily by

the hydrological regime and the materials that make up the bed of the stream channel. To begin with a general discussion of monitoring procedures is given in this introduction. Subsequent sections explain the physical characteristics of streams that are important in measuring fish habitat values, followed by survey methods and assessment procedures.

A monitoring program to assess instream work is a crucial part of any stream restoration project since it allows the assessment of how effective the restorative measures are in the future and may suggest improved methods if a particular measure does not work very well. Ideally, a monitoring program should include the following basic components:

- Survey before any restoration work has taken place to determine the existing state of the stream.
- Survey of restored stream immediately after restoration work has been completed (asbuilt survey).
- Periodic surveys after restoration to determine changes to the restored section of stream (Ideally annually just after major floods).

The data collected during this basic procedure is then used to assess the following:

- Determination of the amount of increased fish habitat due to the initial restoration works. This is achieved by comparing the surveys before and immediately after instream works.
- Determination of changes in the amount of fish habitat over a period of time after restoration works. This is achieved by comparing the subsequent surveys with the survey immediately after restoration works were completed, and determines the stability of the restoration works.

The purpose of the monitoring is to determine absolute changes in amounts of fish habitat, which is hopefully improved, and by implication the attendant changes in numbers of fish utilizing the habitat. A second aim is to determine the effectiveness of different restoration measures and provide feedback to improve their implementation in the future. In addition, the information collected can also be used to calculate the efficiency of different restorative measures by relating absolute improvements in fish habitat to the money spent to achieve those gains. This will suggest which methods provide the best value for money in a given situation.

The general discussion in this section has presented the fundamental components of any monitoring program. Before discussing the various types of survey possible and the assessment procedures in more detail, the next section contains a general discussion of stream morphology which ultimately determines the quality of fish habitat in a stream.

### Stream Morphology

Various channel properties within watersheds can be used to determine channel morphology (Hogan and Ward, 1997). The most important properties are bankfull width  $(W_b)$ , bankfull depth (d), maximum bed sediment size (D) and gradient (s). The Channel

Assessment Procedure (CAP) uses these parameters to classify stream channels into three classes (Anon, 1996a; 1996b):

- Riffle-pool morphology
- Cascade-pool morphology
- Step-pool morphology

These three morphologies tend to be found in sequence throughout a watershed. Rifflepool in the low gradient (< 4%) sections of the lower watershed, cascade-pool in the intermediate gradient (between 4 and 10%) section of the middle watershed and steppool in the high gradient (> 10%) section of the headwaters. Riffle-pool morphologies are used by trout and salmon species (pink, chum, coho and sockeye), cascade-pool morphologies are used by trout, char and a few salmon species (chinook and coho), while step-pool morphologies tend to used by resident trout and char. The most important morphologies for fish that are often degraded during forest harvesting are riffle-pool and cascade-pool, and these are usually the target of restoration work.

Once the channel morphology has been identified there are several measures which characterize the physical properties of stream. The most important are:

- Channel width
- Channel depth (both deeper pool areas and shallower riffles or cascades)
- Wetted width and water depth
- Percentage of riffle and pool or cascade and pool areas (depends on water level)
- Channel bed material
- Woody debris

The combination of these stream attributes determine fish habitat quality in association with factors such as instream vegetation and overbank vegetation. Any monitoring program should include the categorization of general channel morphology together with more detailed physical information that helps to quantify the amount and quality of fish habitat at the time of the survey.

### Survey Methods

Different types of survey may be used to collect data to be used in the assessment procedure. Several levels of data collection are proposed below.

- Qualitative data collection. Setting up of repeatable ground-based photographic stations for recording oblique views, both upstream and downstream, of the site. In addition, aerial photography should be collected. Province of BC aerial photography is often collected at a scale of 1:15,000 that gives some information on surrounding areas to the site, but is not ideal for monitoring purposes since the scale is so small. Aerial photography by low-level helicopter (~1:5,000) should be obtained.
- Semi-quantitative data collection. Combine photographic data with some quantitative measures (e.g. measurement of W<sub>b</sub>, d, D and s to determine channel morphology with

CAP) and qualitative data to determine stability and sediment loading (e.g. field indicators such as eroding banks).

• Quantitative data collection. Collect quantitative data to reflect absolute changes in channel morphology between surveys. Most of these measures can be collected with simple field equipment (e.g. measuring tape and stadia rod) although the level of accuracy, especially the spatial coordinates, is limited. Therefore, it is suggested that more sophisticated survey equipment be used (e.g. total station) so that accurate horizontal and vertical coordinates (with accuracy of at least 5 centimeters) can be recorded for each survey for relation to a set of control points set up during the first survey.

Upstream and downstream of the site record the following parameters at a minimum in a cross-section through the middle of each pool and riffle/cascade crest:

- Distance between cross-sections
- Elevation of top of banks
- Bankfull and wetted channel width
- Bankfull channel depth in deepest part of channel, at edge of wetted width, on top of any gravel bars and channel edges (i.e. topographic cross-section)
- Maximum water depth
- Maximum sediment size (average of b-axis of ten largest sediment grains)

Also, record the upstream and downstream extents of each pool and riffle/cascade sub-unit morphology. Ideally, more intensive data sampling than the minimum suggested above should be undertaken. Finally survey the thalweg (deepest portion) of the streambed and water surface from at least 200 meters upstream of the site to 200 meters downstream. Include enough detail to represent variations in gradient along the channel.

An important component of many stream restoration projects is the inclusion of LWD or boulders in the channel. As part of the survey some or all of these installed components should be identified and tagged and their location determined in 3-D (boulder top or both ends of a piece of LWD). Boulders are especially difficult to identify but may be painted with bright metallic paint to help later identification with a metal detector. Other methods include drilling a hole and gluing in a piece of metal. The coordinates of these installed components should subsequently be monitored in addition to stream parameters. This enables the distance of travel for different sized installed components to be determined which indicates the downstream impact.

Obviously, the site that is to be/has been restored has to be surveyed but, in addition, a significant distance upstream and downstream (200 meters or more for small-scale works) should also be surveyed to determine the surrounding impacts of restoration work.

#### Assessment Procedures

Once survey data has been collected a variety of options are available to help determine the effectiveness of instream works.

- Qualitative. Description of changes based on a sequence of air photos, preferably at a large scale (1:5,000), so that individual logs and riffle-pool or cascade-pool sequences can be identified. In addition, a series of on-the-ground oblique photos of the stream works should be taken from the same point and in the same direction each time. This will provide a time-lapse record of both the site and the downstream impact (good or bad) of the stream restoration works. It will be possible to use the aerial photos to make some quantitative measures of changes in stream parameters (e.g. stream width and locations of LWD that has moved between surveys). In addition, qualitative descriptions of site conditions could be made by the field crew taking the ground photos.
- Semi-quantitative. Quantitative classification of stream morphology change, qualitative description of changes in fish habitat, sediment load etc. This would involve following the CAP procedure to quantitatively assess channel morphology and qualitatively assess whether the system is stable or unstable (aggrading or degrading). The CAP field procedure uses a series of field indicators to qualitatively assess the stability of the stream with reference to a series of keys into one of seven classes (3 degrading, stable and 3 aggrading). The stability class is related to fish habitat quality. As a general rule, stable morphologies have the highest quantity and quality of fish habitat and as the system becomes more degraded/aggraded, the quality and quantity decrease.
- Quantitative. Quantitative description of changes in fish habitat, sediment load etc. This would involve using the quantitative survey data to calculate absolute changes in the following which is possible from the data collected as outlined above.
  - Channel width and depth
  - Areas of pool and riffle/cascade (which depends upon water level)
  - Water depth
  - Sediment stored in the channel and in bars
  - Sediment size
  - Changes in channel location due to bank erosion

This data will give quantitative data to indicate whether the stream channel is stable, aggrading or degrading. In particular, a sediment budget for the surveyed sections can then be calculated that shows the absolute changes in sediment storage between surveys.

#### Discussion

There are many options available when designing and implementing a monitoring program. Ultimately, the level of assessment required (i.e. qualitative verses quantitative) and the length of the monitoring program will determine the budget required to allow proper implementation. All monitoring situations are different but a general amount of baseline information should be collected for all sites. This should include repeatable photography at the very least and ideally some form of instream survey over a period of at least 5 - 10 years. The periodic repeating of a CAP will give a good general idea as to the changing physical state of the stream that will indicate when restoration measures

have been effective. The greater effort put into collecting quantitative data will be primarily rewarded by contributing to basic research to assess the fundamentals of stream restoration measures and the dynamics of streams.

### Results

The data gathered to date includes

- photographs taken on October 15 from various locations (see Appendix A),
- the original FHAP data (Giesbrecht et al, 1998) that was gathered during August, 1997 on fish and fish habitat condition,
- topographic survey data gathered during August, 1997, during the initial preconstruction design phase, along with the associated construction drawing (see Appendix B).
- as built survey data gathered November 7, 1998, including data to construct a longitudinal profile of the thalweg, wetted edges and cross sections, along with the associated as-built drawing (see Appendix C).
- an assessment of the construction by Ministry of Environment biological staff (Fillier and Lough 1999).
- an assessment of the sites and the plans for restorative treatment by a biologist from the US Forest Service (Harkleroad 1998).
- a centreline survey conducted by Cedarvale Resources Ltd. during March, 1999 (see Appendix F).

Permanent reference points for photography were installed in the form of 2 cm x 2 cm x 2 m steel posts driven into the ground to a convenient camera height. These photo points were then tagged with identifying metal tags and their locations were determined using a total station. Locations were chosen such that all structures could be viewed from one or the other of these points. Two such photo points were established at Site 14 and three at Site 15.

Jeff Lough and Darren Fillier, from the Ministry of Environment, Lands and Parks (MoELP), visited the site on November 12, after construction was complete. They have summarized their assessment of the work done at the site in the form of a letter dated March 8, 1999 (see attached copy).

In this letter they expressed concern regarding Site 14 with respect to the pull back of banks, inadequate seeding with grass, loss of low shrub and herb cover, inadequate step pool construction using insufficiently sized and improperly oriented materials and inadequate regulatory agency approvals.

With respect to Site 15, they suggested that, although the LWD was of high quality, branches and tops should be left attached. They further suggested that the LWD be anchored. Concerns were expressed over the stability of the debris catchers, possible end scouring around a channel spanning piece of LWD, riparian area degradation by machine use and the channel excavation.

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Sites 14 and 15 were also visited during late September of 1998 before construction, by Jeff Lough and Darren Fillier from the MoELP, and Glenn Harkleroad, a Fisheries Biologist working with the U.S. Forest Service. In a summary of his observations (see attached copy), Mr. Harkleroad suggested that Site 14 was a low priority site, that the fish habitat in this stream was of limited value and that placement of wood in the stream would not likely improve it. Regarding Site 15, Mr. Harkleroad suggested experimenting with anchoring techniques and directing the flow away from the southern bank using log structures.

In addition to the methods outlined in the Monitoring Plan above, particular attention should be paid during the monitoring program to the items of concern addressed above.

The amount of preliminary data gathered was limited by many factors, including the lateness of the season, which resulted in poor fishing success for juvenile fish, and the presence of snow, making visual assessment practically impossible.

### Recommendations

It is recommended that the Monitoring and Evaluation program be incorporated as a regular part of the overall watershed restoration program. The activities described above should be scheduled into a five year long plan and this work should be budgeted adequately. The work should be integrated with similar monitoring work in other parts of this and the Kitseguecla watershed so that efficiencies of scale can be realized.

It is recommended that the LWD installed at Site 15 should be anchored to imported boulders >65 cm in their b axis, using steel cable >1.5 cm in diameter epoxied into 15 cm deep holes drilled into the rock using the Hilti Epoxy system. Such boulders may be available along the west Kitwancool Lake FSR.

### References

- Fillier, D. and J. Lough. 1999. Letter to Bill Fell dated March 8, 1999. A copy is attached to this report as Appendix D.
- Giesbrecht, S., G. Grieve and M. Prins. 1998. Level I detailed assessment of fish and fish habitat in the south Kitwanga River and its tributaries. Report for the Gitsegukla Band Council, available at the Regional Library, Ministry of Environment, 3726 Alfred Ave., Smithers, B.C.
- Gilchrist, A. 1998. Kitwanga River and Kitseguecla River Watershed Restoration Program: Hydrological and channel stability assessments of specific impact sites. Prepared for the Gitsegukla Band Council.
- Harkleroad, G.R. 1998. British Columbia Stream Restoration Project Review Report, 1998. A copy is attached to this report as Appendix E.
- Wildstone Resources Ltd. 1995. Level I Assessment of the Kitwanga River Watershed. Prepared for Skeena Cellulose Inc. Available in the library, Ministry of Environment, 3726 Alfred Ave., Smithers, B.C., V0J 2N0

Appendix A. Photographs.

Site 14



Photo 1. This mosaic looks north during the construction at Site 14. Visible from the perched culvert downstream, are the excavated plunge pool, a small rock weir, another plunge pool and the pulled back bank.

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Photo 2. Looking downstream from atop the perched culvert. The upstream limit of treatment was located at the red flag, where a cluster of complete trees was prescribed with root wads upstream.



Photo 3. An aerial view of Site 15.



Photo 4. Looking upstream toward the complete tree with root wad attached that was one of two pieces of LWD that were installed across the channel.



Photo 5. Looking downstream. The technicians are standing on the LWD installed furthest upstream.

Appendix B. Pre-Construction Survey Data and Drawings.

| This site is ~ 19 m lo | Constructio    | Site 14 Pre-Construction Survey Data This site is ~ 19 m long from the culvert lip to the mainstem Kitwanga The thalweg has <1 m sinuosity. |  |
|------------------------|----------------|---------------------------------------------------------------------------------------------------------------------------------------------|--|
| The channel            | is incised     | The channel is incised ~ 2 m below an old road grade in fine material.                                                                      |  |
| The channel is ~       | is ~ 2 m at Wb | tt Wb                                                                                                                                       |  |
| X-Section @            | 5 m below      | X-Section @ 5 m below culvert, starting from s side                                                                                         |  |
| 0                      | 3.6            |                                                                                                                                             |  |
| 5                      | 3.5            |                                                                                                                                             |  |
| 7                      | 2.4            |                                                                                                                                             |  |
| 80                     | 2.2            |                                                                                                                                             |  |
| 6                      | 0.4            |                                                                                                                                             |  |
| 10                     | 0              |                                                                                                                                             |  |
| 12                     | 0              |                                                                                                                                             |  |
| 13                     | 0.4            |                                                                                                                                             |  |
| 14                     | 2.2            |                                                                                                                                             |  |
| 15                     | 2.4            |                                                                                                                                             |  |
| 16                     | 3.5            |                                                                                                                                             |  |
| 21                     | 3.6            |                                                                                                                                             |  |



Figure 2. Construction drawing for Site 14, Kitwanga River.

| Survey of KI  | itwanga Pr               | Survey of Kitwanga Prescription Site 15 using clino | 5 using clinon                   | er, comp    | pass and t   | ape.                                |           |     | - |           |           | Ę       |
|---------------|--------------------------|-----------------------------------------------------|----------------------------------|-------------|--------------|-------------------------------------|-----------|-----|---|-----------|-----------|---------|
| Shot Com      | Comment                  | Slope Distance % Slope                              |                                  | НО          | HA           |                                     |           |     |   |           |           | ٨IJ     |
| 9e            |                          | -                                                   |                                  | E           | deg          | min                                 | Dec Deg   | sec |   | Dec Deg   | Dec Brg   | E       |
|               |                          |                                                     | 1                                |             | -            |                                     |           |     |   |           |           |         |
| POC is a me   | a metal tag facing east, |                                                     | nailed to a 20 cm DBH cottonwood | BH cottonv  | poon         |                                     |           |     | + |           |           |         |
| located on th | he north bi              | located on the north bank above the cree's mouth.   | 100                              | Reference p | oint is at t | Reference point is at base of tree. |           |     | - |           |           |         |
| POC Desc      | Description              |                                                     |                                  |             |              |                                     |           |     |   |           |           |         |
| 1 to mo       | 1 to mouth of cr.        | 15.8                                                | -19                              | 15.6244     | 168          |                                     | 0.00000   | 0   | 0 | 0.00000   | 168.00000 | -2.3490 |
| 2 s bar       | s bank at mou            | 16.6                                                | -10                              | 16.5488     | 152          |                                     | 0.00000   | 0   | 0 | 0.00000   | 152.00000 | -1.3024 |
|               |                          | 8.5                                                 | -20                              | 8.3954      | 176          |                                     | 0 0.00000 | 0   | 0 | 0.00000   | 176.00000 | -1.3297 |
| move          | moved to sta 1           | (mouth)                                             |                                  |             |              |                                     |           |     | - |           |           |         |
| 4             |                          | 7.75                                                | 4                                | 7.7462      | ~            |                                     | 0 00000   | 0   | 0 | 0.00000   | 8.00000   | 0.2434  |
| 5             |                          | 19.6                                                | 4                                | 19.5903     |              | 6                                   | 0.0000.0  | 0   |   | 0.00000   | 9.00000   | 0.6157  |
| move          | moved to sta 4           |                                                     |                                  |             |              |                                     |           |     | - |           |           |         |
| 9             |                          | 15.4                                                | 2.5                              | 15.3970     |              | 4                                   | 0.0000    | 0   |   | 0.00000   | 64.00000  | 0.3024  |
| 2             |                          | 9.2                                                 | 2.5                              | 9.1982      | 73           | 3                                   | 0.00000   | 0   |   | 0.00000   | 73.00000  | 0.1806  |
| . ∞           |                          | 4.9                                                 | 10                               | 4.8849      | 314          | 4                                   | 0.00000   | 0   |   | 0.00000.0 | 314.00000 | 0.3844  |
| 0             |                          | 12.9                                                | 27                               | 12.6110     | 314          | 4                                   | 0.00000   | 0   |   | 0.00000   | 314.00000 | 2.7151  |
| 10            |                          | 18                                                  | 20                               | 17.7784     | 314          | 4                                   | 0.0000    | 0   |   | 0.00000   | 314,00000 | 2.8158  |
| 11            |                          | 13                                                  | 20                               | 12.8399     | 344          | 4                                   | 0.00000   | 0   |   | 0.00000   | 344.00000 | 2.0336  |
| 12            |                          | 13.3                                                | 20                               | 13.1363     |              | 4                                   | 0.00000   | 0   |   | 0.00000   | 4.00000   | 2.0806  |
| 1 67          |                          | 12.6                                                | 11                               | 12.5530     | 18           | 8                                   | 0.00000   | 0   |   | 0.00000   | 18.00000  | 1.0872  |
|               | e side of old ro         | 13.2                                                | 8                                | 13.1740     | 29           | 6                                   | 0.0000    | 0   | - | 0.00000   | 29.00000  | 0.8288  |
|               | stump in ch              | 9.2                                                 | 5                                | 9.1929      | 30           | 0                                   | 0.00000   | 0   | - | 0.00000   | 30.00000  | 0.3612  |
| 5             |                          | 8.9                                                 | 14                               | 8.8463      | 51           | 1                                   | 0.00000   | 0   |   | 0.00000   | 51.00000  | 0.9766  |
| 17            |                          | 2.1                                                 | 44                               | 1.9758      | 144          | 4                                   | 0.00000   | 0   |   | 0.00000   | 144.00000 | 0.7113  |
| 18            |                          | 10.3                                                | 12                               | 10.2543     | 144          | 4                                   | 0.00000   | 0   |   | 0.00000   | 144.00000 | 0.9693  |
| 19            |                          | 12.1                                                | 28                               | 11.8086     | 142          | 2                                   | 0.00000   | 0   |   | 0.00000   | 142.00000 | 2.6395  |
| move          | moved to sta 1           | 5 at stump                                          |                                  |             |              |                                     |           |     |   |           |           | 00100   |
| 20            |                          | 9.4                                                 | -                                | 9.3997      |              | 72                                  | 0.00000   | 0   | - | 0.00000   | 72.00000  | 0.0738  |
|               | on bank above            | 9.7                                                 | 11                               | 9.6638      |              | 78                                  | 0.00000   | 0   | - | 0,00000   | 78.00000  | 0.8370  |
| 22            |                          | 18.5                                                | 3                                | 18.4949     |              | 54                                  | 0.00000   | 0   |   | 0.00000   | 54.00000  | 0.4359  |
|               | moved to sta 2           | 22                                                  |                                  |             |              |                                     |           |     |   |           |           | CLTT C  |
| 23 junction   | tion                     | 5.9                                                 | 2.5                              | 5.8989      |              | 7                                   | 0.00000   | 0   | - | 0.0000    | 357.00000 | 0.1138  |
| 24            |                          | 10.1                                                | 5                                | 10.0922     |              | 0                                   | 0.00000   | 0   |   | 0.00000   | 360.00000 | 0.3965  |
| 20            |                          | OV                                                  | U.                               | 4 8946      | 316          | 9                                   | 0.00000   | 0   |   | 0.00000   | 316.00000 | 0.2308  |

| Pole Heigh HI | E       | X=easting | Y=northing | Z     |
|---------------|---------|-----------|------------|-------|
| E             | ш       | m         | ш          | E     |
| Earl          | Glenn   |           |            |       |
|               |         | X         | ×          | 2     |
|               |         | ×         | y          | Z     |
| 1.70000       | 1.70000 | 3.2485    | -15.2830   | -2.35 |
| 1.70000       | 1.70000 | 7.7692    | ì          | -1.30 |
| 1.70000       | 1.70000 | 0.5856    | -8.3749    | -1.33 |
| 1.70000       | 1.70000 | 4.3266    | -7.6122    | 0.24  |
| 1.70000       | 1.70000 | 6.3131    | 4.0661     | 0.62  |
| 1.70000       | 1.70000 | 18.1654   | -0.8626    | 0.30  |
| 1.70000       | 1.70000 | 13.1229   | -4.9229    | 0.18  |
| 1.70000       | 1.70000 | 0.8127    | 1          |       |
| 1.70000       | 1.70000 | -4.7450   |            |       |
| 1.70000       | 1.70000 | 1         |            |       |
| 1.70000       | 1.70000 |           |            | 2.03  |
| 1.70000       | 1.70000 | 5.2429    | 5.4921     | 2.08  |
| 1.70000       | 1.70000 | 8.2057    |            |       |
| 1.70000       | 1.70000 | 10.7135   | 3.9100     |       |
| 1.70000       | 1.70000 | 8.9231    |            |       |
| 1.70000       | 1.70000 | 11.2014   | -2.0451    | 0.98  |
| 1.70000       | 1.70000 | 5.4880    | -9.2107    | 0.71  |
| 1.70000       | 1.70000 | 10.3539   | -15.9081   | 0.97  |
| 1.70000       | 1.70000 | 11.5967   | -16.9175   | 2.64  |
| 1.70000       | 1.70000 | 17.8628   | 3.2538     | 0.07  |
| 1.70000       | 1.70000 | 18.3757   | 2.3583     | 0.84  |
| 1.70000       | 1.70000 | 23.8858   | 11.2201    | 0.44  |
| 1 70000       | 1.70000 | 23.5771   | 17.1109    | 0.12  |
| 1.70000       |         | 23.8858   | 3 21.3123  |       |
| 1 70000       | 1 70000 | 20.4858   | 14,7410    | 0.23  |

| 26               | 14.4 | 9   | 14.3840 | 315 | 0.00000 | 0.00000 | 315.00000 | 0.6783 |
|------------------|------|-----|---------|-----|---------|---------|-----------|--------|
| 07 too of honk   | 18.0 | 10  | 18 6900 | 318 | 0.00000 | 0.00000 | 318.00000 | 2.8099 |
|                  | P'OI | 2 4 | 23 8336 | 318 | 0.00000 | 0.00000 | 318.00000 | 2.8209 |
| Zo DITI Dack     | t 7  | 00  | 1 1821  | 141 | 0.00000 | 0.00000 | 141.00000 | 0.2063 |
| 29 S Dank at mou | 4 00 | 25  | 3 2366  | 144 | 0.00000 | 0.00000 | 144.00000 | 0.6438 |
| 30               | 2.0  | 30  | 6 9038  | 144 | 0.00000 | 0.00000 | 144.00000 | 1.6575 |
| 31               | 1.1  |     | 11 8803 | 139 | 0.00000 | 0.00000 | 139.00000 | 1.6908 |
| 32               | 71   | 2 0 | 2000111 | 00  |         | 0.00000 | 00000.06  | 0.1759 |
| 33               | 2.11 | 7 0 | 0.0000  | 30  |         | 00000   | 106.00000 | 0.1555 |
| 34               | 9.9  | N   | 9.8988  | 100 | 0,00000 | 000000  | 200000    | 2 5266 |
| 35               | 10.2 | 32  | 9.8795  | 58  | 0.0000  | 0,0000  | 0000000   |        |
| 36               | 17.2 | 38  | 16.4396 | 58  | 0.00000 | 0.00000 | 58.00000  | 5.05/5 |

| 5.06 | 19.9318 | 37.8274 | 1.70000 | 1.70000 |
|------|---------|---------|---------|---------|
| 2.54 | 16.4555 | 32.2641 | 1.70000 | 1.70000 |
| 0.16 | 8.4916  | 33.4011 | 1.70000 | 1.70000 |
| 0.18 | 11.2201 | 35.0844 | 1.70000 | 1.70000 |
| 1.69 | 2.2539  | 31.6800 | 1.70000 | 1.70000 |
| 1.66 | 5.6348  | 27.9438 | 1.70000 | 1.70000 |
| 0.64 | 8.6016  | 25.7882 | 1.70000 | 1.70000 |
| 0.21 | 10.3014 | 24.6297 | 1.70000 | 1.70000 |
| 2.82 | 28.9319 | 7.9380  | 1.70000 | 1.70000 |
| 2.81 | 25.1094 | 11.3798 | 1.70000 | 1.70000 |
| 0.68 | 21.3911 | 13.7148 | 1.70000 | 1.70000 |



Figure 2. Pre-Construction plan for Site 15.

Appendix C. As-Built Survey Data and Drawings.

|              |                                                                                                        |                 |        | 2             |       | lotal station same and of the same shows the same shows a state of the |          |          |         |            |          |             |
|--------------|--------------------------------------------------------------------------------------------------------|-----------------|--------|---------------|-------|------------------------------------------------------------------------|----------|----------|---------|------------|----------|-------------|
| ioLith S     | BioLith Scientific Consultants Inc                                                                     | nsultan         | ts Inc |               |       |                                                                        |          |          |         |            |          |             |
| 250-635-5378 |                                                                                                        | Temp            |        | 6             |       |                                                                        |          |          |         |            |          |             |
|              |                                                                                                        | <b>WX</b>       | cool   | cool overcast |       |                                                                        |          |          |         |            |          |             |
|              |                                                                                                        | Date of Survey: | Surv   | 'ey:          |       | Nov.2                                                                  | 1998     |          |         |            |          |             |
| Crew         |                                                                                                        |                 |        |               |       |                                                                        |          |          |         |            |          |             |
| entax        | Pentax PCS 325-W Barom Presi 986                                                                       | Barom           | Pres   | 986           |       |                                                                        |          |          |         |            |          |             |
| II meas      | All measurements taken from BM#48.                                                                     | aken fro        | m BN   | <u>1#48.</u>  |       |                                                                        |          |          |         |            |          |             |
| loaci re     | Measurements to I aree Woody Debris pieces taken with respect to nails driven into each end of the log | Inde Wo         | vboc   | Debri         | s pie | ces taken                                                              | with res | spect to | nails d | riven into | each end | of the log. |
| leasur       | Measurements to photo points taken to the top of the reference post or metal pipe.                     | noto poi        | nts ta | aken t        | o the | top of the                                                             | referel  | nce post | or me   | tal pipe.  |          |             |
| lissing      | Missing shot numbers indicate no data recorded                                                         | rs indic        | ate n  | o dati        | a rec | orded.                                                                 |          |          |         |            |          |             |
| Chot #       | Description HD                                                                                         | GH              | HA     |               |       | Decimal                                                                | VD       | RH       | Ŧ       |            |          |             |
| 1011         | 2                                                                                                      |                 | Degl   | Minu          | Secu  | Dear Minu Seci Dearees                                                 |          |          |         | ×          | y        | z           |
| C            | BM48 & SP                                                                                              |                 | 0      |               |       | 2                                                                      |          |          |         | 0.000      | 0.000    | 0.000       |
|              | -                                                                                                      | 15.16           | 143    | 20            | 45    | 143.346                                                                | -0.82    | 1.676    | 1.66    | 9.050      | -12.162  | -0.840      |
| 2            |                                                                                                        | 16.82           | 169    | 51            | 50    | 169.864                                                                | -0.24    | 1.676    | 1.66    | 2.960      | -16.557  | -0.260      |
| 10           |                                                                                                        | 13.63           | 129    | 11            | 50    | 129.197                                                                | -3.13    | 1.676    | 1.66    | 10.563     |          | -3.150      |
| 4            |                                                                                                        | 11.54           | 138    | 38            | 20    | 138.639                                                                | -3.41    | 1.676    | 1.66    | 7.626      |          | -3.430      |
| 2            | Culvert Lip                                                                                            | 14.18           | 116    | 46            | 35    | 116.776                                                                | -2.60    | 1.674    | 1.66    | 12.660     | -6.388   | -2.618      |
| 9            |                                                                                                        | 13.83           | 117    | 51            | 35    | 117.86                                                                 | -3.57    | 1.676    | 1.66    | 12.227     | -6.463   | -3.590      |
| 2            | _                                                                                                      | 13.17           |        |               | 25    | 121.774                                                                | -4.03    | 1.676    | 1.66    | 11.196     | -6.935   | -4.050      |
| . 00         |                                                                                                        | 12.28           |        | 41            | 30    | 125.692                                                                | -3.55    | 1.674    | 1.66    | 9.973      |          | -3.568      |
| 0            |                                                                                                        | 11.09           |        | 2             | 30    | 133.042                                                                | -3.92    | 1.674    | 1.66    | 8.105      |          | -3.938      |
| 10           | TH 5                                                                                                   | 9.88            |        | 6             | 30    | 134.158                                                                | -4.31    | 1.674    | 1.66    | 7.088      |          | -4.328      |
| 11           | TH 6                                                                                                   | 8.8             | 141    | 41            | 20    | 141.689                                                                | -3.69    | 1.76     | 1.66    | 5.455      |          | -3.794      |
| 12           | TH 7                                                                                                   | 8.56            | 147    | 25            | 30    | 147.425                                                                | -3.80    | 1.76     | 1.66    | 4.609      |          | -3.904      |
| 13           | 5 TH 8                                                                                                 | 8.59            | 159    | 38            | 0     | 159.633                                                                | -3.83    | 1.76     | 1.66    |            |          | -3.934      |
| 14           | TH 9                                                                                                   | 8.58            | 159    | 42            | 25    | 159.707                                                                | -3.83    | 1.76     | 1.66    |            |          | -3.934      |
| 15           | 15 TH 10                                                                                               | 10.13           | 177    | 38            | 50    | 177.647                                                                | -4.41    | 1.76     | 1.66    | 0.416      | 1        | -4.514      |
| 16           | 16 TH 11                                                                                               | 10.02           | 185    | 28            | 40    | 185.478                                                                | -4.57    |          |         |            | -9.974   | -4.674      |
| 17           | 7H 12                                                                                                  | 9.81            | 192    | S             | 55    | 192.065                                                                | -4.58    | 1.76     |         |            | -9.593   | -4.684      |
| 18           | 18 TH 13                                                                                               | 11.07           | 209    | 37            | 0     | 209.617                                                                | -4.86    | 1.76     |         |            |          | -4.964      |
| 19           | 19 TH 14                                                                                               | 11.68           | 216    | 56            | 15    | 216.938                                                                | -4.94    |          |         | -7.019     | -9.336   | -5.044      |
|              |                                                                                                        |                 |        |               |       |                                                                        |          |          |         |            |          |             |

| -0.004     | -3.434     | -3.404     | -3.354     | -3.324     | -3.704     | -3.734     | -3.784     | -3.884     | -3.844      | -4.194      | -4.264      | -4.350      | -4.490      | -4.750      | -4.790      | -5.290      | -5.360      | -5.246       | -4.856      | -4.756      | -4.716      | -4.356      | -4.046      | -3.836      | -3.856      | -3.756      | -3.636      | -3.656      | -3.626      | -3.476      | -3.266      | -3.306      | -3.276      | -3.296      | -0.046      |
|------------|------------|------------|------------|------------|------------|------------|------------|------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|--------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| ?          | ကို         | 4           | 4           | 4           | 4           | 4           | 4           | Ŷ           | 2           | 2            | 4           | 4           | 4           | 4           | 4           | ကို         | ကို         | ဂု          | ę           | ကို         | ę           | ကု          | ကို         | ဂု          | ကု          | ကု          | 9           |
| -0.9/0     | -7.928     | -8.412     | -8.135     | -7.202     | -7.954     | -8.134     | -7.285     | -7.871     | -8.644      | -8.405      | -10.246     | -10.329     | -10.311     | -10.325     | -9.654      | -10.995     | -11.772     | -10.125      | -8.361      | -8.851      | -9.137      | -9.178      | -7.893      | -6.881      | -6.373      | -6.824      | -6.268      | -5.704      | -5.965      | -7.027      | -6.911      | -5.496      | -5.287      | -5.722      | -34.660     |
| 017.21     | 12.284     | 11.040     | 10.229     | 9.922      | 8.444      | 6.497      | 5.683      | 4.466      | 3.694       | 3.047       | 0.832       | -0.663      | -3.004      | -5.440      | -6.157      | -11.500     | -12.650     | -12.787      | -6.931      | -5.479      | -4.601      | -0.460      | 2.222       | 3.009       | 3.954       | 4.708       | 5.622       | 7.013       | 7.599       | 8.836       | 9.724       | 10.056      | 11.492      | 12.536      | 11.757      |
| 1.66       | 1.66       | 1.66       | 1.66       | 1.66       | 1.66       | 1.66       | 1.66       | 1.66       | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66         | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        | 1.66        |
| 1./5       | 1.75       | 1.75       | 1.75       | 1.75       | 1.75       | 1.75       | 1.75       | 1.75       | 1.75        | 1.75        | 1.75        | 1.656       | 1.656       | 1.656       | 1.656       | 1.656       | 1.656       | 1.652        | 1.652       | 1.652       | 1.652       | 1.652       | 1.652       | 1.652       | 1.652       | 1.652       | 1.652       | 1.652       | 1.652       | 1.652       | 1.652       | 1.652       | 1.652       | 1.652       | 1.652       |
| -3.27      | -3.34      | -3.31      | -3.26      | -3.23      | -3.61      | -3.64      | -3.69      | -3.79      | -3.75       | -4.10       | -4.17       | -4.35       | -4.49       | -4.75       | -4.79       | -5.29       | -5.36       | -5.25        | -4.86       | -4.76       | -4.72       | -4.36       | -4.05       | -3.84       | -3.86       | -3.76       | -3.64       | -3.66       | -3.63       | -3.48       | -3.27       | -3.31       | -3.28       | -3.30       | -0.05       |
| 118.768    | 122.84     | 127.306    | 128.494    | 125.974    | 133.289    | 141.382    | 142.042    | 150.429    | 156.863     | 160.069     | 175.357     | 183.674     | 196.244     | 207.785     | 212.528     | 226.286     | 227.06      | 231.628      | 219.658     | 211.758     | 206.726     | 182.871     | 164.276     | 156.383     | 148.182     | 145.399     | 138.114     | 129.125     | 128.131     | 128.494     | 125.401     | 118.657     | 114.704     | 114.535     | 161.263     |
| 2          | 25         | 20         | 40         | 25         | 20         | 55         | 30         | 45         | 45          | 10          | 25          | 25          | 40          | 2           | 40          | 10          | 35          | 40           | 30          | 30          | 35          | 15          | 35          | 0           | 55          | 55          | 50          | 30          | 50          | 40          | 2           | 25          | 15          | 5           | 45          |
| 46         | 50         | 18         | 29         | 58         | 17         | 22         | 2          | 25         | 51          | 4           | 21          | 40          | 14          | 47          | 31          | 17          | e           | 37           | 39          | 45          | 43          | 52          | 16          | 23          | 10          | 23          | 9           | 2           | 2           | 29          | 24          | 39          | 42          | 32          | 15          |
| 118        | 122        | 127        | 128        | 125        | 133        | 141        | 142        | 150        | 156         | 160         | 175         | 183         | 196         | 207         | 212         | 226         | 227         | 231          | 219         | 211         | 206         | 182         | 164         | 156         | 148         | 145         | 138         | 129         | 128         | 128         | 125         | 118         | 114         | 114         | 161         |
| 14.5       | 14.62      | 13.88      | 13.07      | 12.26      | 11.6       | 10.41      | 9.24       | 9.05       | 9.4         | 8.94        | 10.28       | 10.35       | 10.74       | 11.67       | 11.45       | 15.91       | 17.28       | 16.31        | 10.86       | 10.41       | 10.23       | 9.19        | 8.2         | 7.51        | 7.5         | 8.29        | 8.42        | 9.04        | 9.66        | 11.29       | 11.93       | 11.46       | 12.65       | 13.78       | 36.6        |
| Wetted Wid | 22 WW RL 2 | 23 WW RL 3 | 24 WW RL 4 | 25 WW RL 5 | 26 WW RL 6 | 27 WW RL 7 | 28 WW RL 8 | 29 WW RL 9 | 30 WW RL 10 | 31 WW RL 11 | 32 WW RL 12 | 33 WW RL 13 | 34 WW RL 14 | 35 WW RL 15 | 36 WW RL 16 | 37 WW RL 17 | 38 WW RL 18 | 39 WW 19 R/F | 40 WW RR 20 | 41 WW RR 21 | 42 WW RR 22 | 43 WW RR 23 | 44 WW RR 24 | 45 WW RR 25 | 46 WW RR 26 | 47 WW RR 27 | 48 WW RR 28 | 49 WW RR 29 | 50 WW RR 30 | 51 WW RR 31 | 52 WW RR 32 | 53 WW RR 33 | 54 WW RR 34 | 55 WW RR 35 | 56 CROSS SE |
| 21 V       | 22 V       | 23 V       | 24 V       | 25 V       | 26 V       | 27 V       | 28 V       | 29 V       | 30 V        | 31 V        | 32 V        | 33 V        | 34 V        | 35 V        | 36 V        | 37 V        | 38 V        | 39 V         | 40 V        | 41 V        | 42 V        | 43 V        | 44 V        | 45 V        | 46 V        | 47 V        | 48 V        | 49 V        | 50 \        | 51 V        | 52 V        | 53 \        | 54 V        | 55 \        | 56 0        |

| 0.114    | -0.376   | -3.546   | -3.786   | -3.526  | 0.104    | 0.004    | -1.256    | -3.676        | -3.776     | -0.726     | -0.396   | -0.926   | -1.296   | -1.026         | -1.436         | -1.726       | -1.286       | -0.046       | -0.346       | -0.606       | -3.770       | -4.110       | -3.760       | -3.720       | -3.740       | -4.320       |
|----------|----------|----------|----------|---------|----------|----------|-----------|---------------|------------|------------|----------|----------|----------|----------------|----------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| -19.360  | -14.476  | -9.734   | -8.216   | -6.645  | -0.142   | 7.137    | 19.500    | -8.873        | -7.498     | -17.625    | -13.531  | -11.488  | -10.069  | -5.817         | -3.237         | -3.522       | -1.822       | 0.761        | -1.484       | -0.109       | -6.666       | -6.699       | -7.093       | -6.274       | -7.870       | -6.904       |
|          |          | 4.146    | 4.072    | 3.477   | 2.025    | -0.950   | -4.262    | 3.895         | 2.489      | -4.617     | 7.162    | 9.567    | 13.059   | 14.205         | 11.254         | 9.594        | 8.333        | 6.526        | -2.596       | -6.309       | 12.288       | 11.328       | 10.643       | 10.846       | 11.482       | 7.179        |
| 1.66     | 1.66     | 1.66     | 1.66     | 1.66    | 1.66     | 1.66     | 1.66      | 1.66          | 1.66       | 1.66       | 1.66     | 1.66     | 1.66     | 1.66           | 1.66           | 1.66         | 1.66         | 1.66         | 1.66         | 1.66         | 1.66         | 1.66         | 1.66         | 1.66         | 1.66         | 1.66         |
| 1.652    | 1.652    | 1.652    | 1.652    | 1.652   | 1.652    | 1.652    | 1.652     | 1.652         | 1.652      | 1.652      | 1.652    | 1.652    | 1.652    | 1.652          | 1.652          | 1.652        | 1.652        | 1.652        | 1.652        | 1.652        | 1.656        | 1.656        | 1.656        | 1.656        | 1.656        | 1.656        |
| 0.11     | -0.38    | -3.55    | -3.79    | -3.53   | 0.10     | 0.00     | -1.26     | -3.68         | -3.78      | -0.73      | -0.40    | -0.93    | -1.30    | -1.03          | -1.44          | -1.73        | -1.29        | -0.05        | -0.35        | -0.61        | -3.77        | -4.11        | -3.76        | -3.72        | -3.74        | -4.32        |
| 158.558  | 159.351  | 156.926  | 153.638  | 152.378 | 94.0181  | 352.415  | 347.672   | 156.3         | 161.639    | 194.681    | 152.108  | 140.213  | 127.635  | 112.268        | 106.046        | 110.158      | 102.336      | 83.3444      | 240.235      | 269.014      | 118.478      | 120.599      | 123.681      | 120.05       | 124.429      | 133.882      |
| 30       | 2        | 35       | 15       | 40      | 2        | 55       | 20        | 0             | 20         | 50         | 30       | 45       | 2        | 2              | 45             | 30           | 10           | 40           | 2            | 50           | 40           | 55           | 50           | 0            | 45           | 55           |
| 33       | 21       | 55       | 38       | 22      | -        | 24       | 40        | 18            | 38         | 40         | 9        | 12       | 38       | 16             | 2              | 6            | 20           | 20           | 14           | 0            | 28           | 35           | 40           | e            | 25           | 53           |
| 158      | 159      | 156      | 153      | 152     | 94       | 352      | 347       | 156           | 161        | 194        | 152      | 140      | 127      | 112            | 106            | 110          | 102          | 83           | 240          | 269          | 118          | 120          | 123          | 120          | 124          | 133          |
| 20.8     | 15.47    | 10.58    | 9.17     |         | 2.03     | 7.2      | 19.96     |               | 7.9        | 18.22      |          | 14.95    | 16.49    | 15.35          | 11.71          | 10.22        | 8.53         | 6.57         | 2.99         | 6.31         | 13.98        | 13.16        | 12.79        | 12.53        | 13.92        | 96.6         |
| 58 C/S 3 | 59 C/S 4 | 60 C/S 5 | 61 C/S 6 | C/S 7   | 63 C/S 8 | 64 C/S 9 | 65 C/S 10 | 66 Iwd U/S TA | 67 LWD D/S | 68 CHANNEL | 69 cb #2 | 70 CB #3 | 71 cb #4 | 72 #5 Top of ( | 73 channel bre | 74 CB r/r #2 | 75 CB R/R #3 | 76 CB r/R #4 | 77 CB R/R #5 | 78 cb R/R #6 | 79 POOL #1-1 | 80 POOL #1-2 | 81 POOL #1-3 | 82 POOL #1-4 | 83 POOL #1-5 | RA POOL #2 F |
| 58       | 59       | 60       | 61       | 62 0    | 63       | 64       | 65        | 66            | 67         | 68         | 69       | 20       | 17       | 72             | 73             | 74           | 75           | 76           | 17           | 78           | 29           | 80           | 81           | 82           | 83           | Va           |



| BioLith Scientific Consultants Inc.<br>250-635-5378 7 7<br>Crew EW/GG 8<br>Pentax PCS 325-W 8<br>All measurements taken from BM All measurements taken from BM Measurements to Large Woody I measurements to photo points ta Missing shot numbers indicate no                                                                                                                                                                                                                                                                                                                                | onsultan  | ts Inc.  |        |             |                           |          |          |         |                                                        |          |            |                                      |  |
|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------|----------|--------|-------------|---------------------------|----------|----------|---------|--------------------------------------------------------|----------|------------|--------------------------------------|--|
| 250-635-5378<br>Crew EW/GG<br>Pentax PCS 325-W<br>All measurements to L<br>Measurements to L<br>Measurements wer<br>Missing shot numb                                                                                                                                                                                                                                                                                                                                                                                                                                                        |           |          | _      | _           |                           |          |          |         |                                                        |          |            |                                      |  |
| Crew EW/GG<br>Pentax PCS 325-W<br>All measurements to L<br>Measurements wer<br>Measurements to p<br>Missing shot numbe                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |           | F        | Temp   |             |                           | 8        |          |         |                                                        |          |            |                                      |  |
| Pentax PCS 325-W     Barom Press.     981       All measurements taken from BM#56.     981       All measurements taken from BM#56.     981       Measurements to Large Woody Debris pieces taken with respect to nails driven in measurements were taken with respect to one nail driven into the highest point on measurements to photo points taken to the top of the reference post or metal pipe Missing shot numbers indicate no data recorded. |           |          |        |             |                           |          |          |         |                                                        |          |            |                                      |  |
| All measurements t<br>Measurements to L<br>measurements wer<br>Measurements to p<br>Missing shot numb                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |           |          | Barom  | Barom Press | ss.                       | 981      |          |         |                                                        |          |            |                                      |  |
| Measurements to Large Woody Debris pieces taken with respect to nails driven into each en<br>measurements were taken with respect to one nail driven into the highest point on the piece.<br>Measurements to photo points taken to the top of the reference post or metal pipe.<br>Missing shot numbers indicate no data recorded.                                                                                                                                                                                                                                                           | taken fro | m BM     | #56.   |             |                           |          |          |         |                                                        |          |            |                                      |  |
| measurements wer<br>Measurements to p<br>Missing shot numb                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | arde Wo   | D vboc   | Debris | ; piece     |                           | th respe | ect to n | ails dr | with respect to nails driven into each end of the log. | each end | of the log | g. Debris catcher                    |  |
| Missing shot numb                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | e taken   | with re  | espec  | t to o      |                           | en into  | the hig  | hest p  | oint on the                                            | e piece. |            |                                      |  |
| Missing shot numbr                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | photo po  | ints tak | ken to | o the t     | top of the re             | sference | e post   | or met  | al pipe.                                               |          |            |                                      |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | ers indic | ate no   | ) data | I recol     | rded.                     |          |          |         | 1                                                      |          |            |                                      |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |           |          |        |             |                           |          |          |         |                                                        |          |            |                                      |  |
| First First SP ta                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | tag #55   |          |        |             |                           |          |          |         |                                                        |          |            |                                      |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |           | Darr     | Vinik  | C D         | Decr. Mini Secc Dec. Dec. | d A      | RH       | Ē       | ×                                                      | X        | Z          | Description                          |  |
| 21101#                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |           |          |        | 2           |                           |          |          |         | 0.000                                                  | 0.000    | 0.000 BM55 | BM55                                 |  |
| 1 to toc # 5/                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 20 74     | 217      | 00     | 35          | 217.143                   | -2.38    | 1.52     | 1.55    | -17.957                                                | -23.707  | -2.346 t   | -2.346 to tag # 54                   |  |
| 2 adda of hid                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 316       | 227      | 42     | 45          |                           | -1.52    | 1.52     | 1.55    | -23.377                                                | -21.262  | -1.486 e   | -1.486 edge of highest bank on N     |  |
| 2 adda of hid                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 23.01     | 235      | 20     | 25          |                           | -1.35    | 1.52     | 1.55    | -18.927                                                | -13.086  | -1.316 e   | -1.316 edge of highest bank on N     |  |
| 4 Adde of hid                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 15.82     | 251      | -      | 35          | 251.026                   | -0.71    | 1.66     | 1.55    | -14.960                                                | -5.144   | -0.822 6   | -0.822 edge of highest bank on N     |  |
| 5 adda of hid                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 6.59      | 252      | 52     | 20          | 252.872                   | -0.46    | 1.66     | 1.55    | -6.298                                                 | -1.941   | -0.572 €   | -0.572 edge of highest bank on N     |  |
| 6 edge of hid                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 2.09      | 282      | 37     | 55          | 282.632                   | 0.13     | 1.66     | 1.55    | -2.039                                                 | 0.457    | 0.018      | 0.018 edge of highest bank on N      |  |
| 7 Adde of hid                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 3.23      | 195      | 30     | 50          | 195.514                   | -1.01    | 1.66     | 1.55    | -0.864                                                 | -3.112   | -1.122 6   | -1.122 edge of highest bank on N     |  |
| 8 edge of hig                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 3.6       | 131      | 53     | 5           | 131.885                   | -0.76    | 1.66     | 1.55    | 2.680                                                  | -2.403   | -0.872     | edge of highest bank on N            |  |
| a edge of hid                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 10.75     | 93       | 59     | 50          | 93.997                    | -0.07    | 1.66     | 1.55    | 10.724                                                 | -0.749   |            | -0.180 edge of highest bank on N     |  |
| 10 wiedae Nis                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 11.47     | 114      | 2      | 40          | 114.128                   | -3.35    | 1.66     | 1.55    | 10.468                                                 | -4.689   |            | -3.460 w.edge N side                 |  |
| 11 w edge N s                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 8.57      | 127      | 34     | 45          | 127.579                   | -3.36    | 1.66     | 1.55    | 6.792                                                  | -5.226   |            | -3.467 w.edge N side                 |  |
| 12 w edge N s                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 6.01      | 148      | 50     | 2           | 148.835                   | -3.49    | 1.65     | 1.55    | 3.110                                                  | -5.143   |            | -3.594 w.edge N side                 |  |
| 13 Outside of                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 8.47      |          | 17     | 50          | 188.297                   | -3.83    | 1.65     | 1.55    | -1.222                                                 | -8.381   | -3.933 (   | -3.933 Outside of first bend         |  |
| 14 alder clumr                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 11.55     |          | 17     | 55          | 185.299                   | -4.12    | 1.65     | 1.55    | -1.067                                                 | -11.501  | -4.223     | -4.223 alder clump                   |  |
| 15 w adra N s                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 18 22     |          | 44     | 45          | 187.746                   | -4.18    | 1.65     | 1.55    | -2.456                                                 | -18.054  | -4.283 \   | -4.283 w.edge N side                 |  |
| 16 w edge N s                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 21.77     |          | 2      | 55          | 191.049                   | -4.15    | 1.65     | 1.55    | -4.172                                                 | -21.366  | -4.253 \   | -4.253 w.edge N side                 |  |
| 17 w edge N s                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 25.4      | 1        | 50     | 50          | 199.847                   | -4.29    | 1.65     | 1.55    | -8.624                                                 |          | -4.393 \   | -4.393 w.edge N side                 |  |
| 18 S and of w                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 24.87     |          | 25     | 20          | 185.422                   | -4.21    | 1.65     | 1.55    | -2.350                                                 |          | -4.310     | -4.310 S end of weir log working u/s |  |
| 19 w. edge S :                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 22.1      |          | 9      | 55          | 182.115                   | -4.2     | 1.6      | 1.55    | -0.816                                                 |          |            | -4.246 w. edge S. side               |  |
| 20 w. edge S :                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 19.94     |          | 14     | 35          | 179.243                   | -4.14    | 1.64     | 1.55    | 0.263                                                  | -19.938  |            | -4.234 w. edge S. side               |  |

|                        |                |                        |                        |                        |                        |                      | edge                                      |                            | ool tail out d/s                                     |                |                |                                |                             |         |                        |                |                       |                 |                        | group of 3-tree #3                           |                           |                      |                |                      |                      |                           |                             |         |                                  |                                  |                                  |                                  |                                  |                                  |                                  |                                  |
|------------------------|----------------|------------------------|------------------------|------------------------|------------------------|----------------------|-------------------------------------------|----------------------------|------------------------------------------------------|----------------|----------------|--------------------------------|-----------------------------|---------|------------------------|----------------|-----------------------|-----------------|------------------------|----------------------------------------------|---------------------------|----------------------|----------------|----------------------|----------------------|---------------------------|-----------------------------|---------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|
| -4.236 w. edge S. side | edge S.        | -3.780 w. edge S. side | -3.488 w. edge S. side | -3.427 w. edge S. side | -3.475 w. edge S. side | 0.766 top of culvert | -1.388 bottom of culvert 2 m in from edge | 2.162 top of photo point 1 | -3.707 thalweg from culvert plunge pool tail out d/s | -3.767 thalweg | -4.157 thalweg | -4.217 u/s of log 1 in thalweg | -2.056 top of photo point 2 | -4.416  | -4.366 middle of log 5 |                | -4.036 N end of log 5 |                 | -3.396 S end of tree 4 | -2.986 rootwad end of S most log of group of | -3.046 middle log-tree #2 | -2.648 N log-tree #1 |                | -2.406 S log-tree #3 | -2.326 N log-tree #1 | -2.966 Middle log-tree #2 | -2.406 N end of crossed log | -3.310  | -1.664 cross section from S to N | -2.323 cross section from S to N | -3.153 cross section from S to N | -4.192 cross section from S to N | -3.692 cross section from S to N | -3.372 cross section from S to N | -3.062 cross section from S to N | -0.950 cross section from S to N |
|                        |                | -10.418 -3             | -7.823 -3              | -9.762 -3              | -7.440                 |                      |                                           |                            |                                                      |                | -              |                                | _                           |         |                        |                |                       |                 |                        |                                              |                           |                      |                | -10.265 -            |                      |                           |                             |         | -18.360 -                        |                                  | -17.531 -                        |                                  |                                  |                                  |                                  | -9.510 -                         |
|                        |                | 2.211                  | 6.229                  | 9.556                  | 12.083                 | 12.881               | 12.685                                    | 15.206                     | 6.660                                                | 3.360          | 0.905          | -0.054                         |                             |         | -4.799                 | -2.483         | -8.008                | -6.027          | 0.991                  | -1.037                                       | 0.460                     | 0.896                | 3.055          | -16.509              | -15.887              | -12.244                   | -10.404                     | -4.966  | 11.455                           | 9.569                            | 7.806                            | 1.465                            | -4.620                           | -11.872                          | -15.800                          | -18.048                          |
| 1.55                   | 1.55           | 1.55                   | 1.55                   | 1.55                   | 1.55                   | 1.55                 | 1.55                                      | 1.55                       | 1.55                                                 | 1.55           | 1.55           | 1.55                           | 1.55                        | 1.55    | 1.55                   | 1.55           | 1.55                  | 1.55            | 1.55                   | 1.55                                         | 1.55                      | 1.55                 | 1.55           | 1.55                 | 1.55                 | 1.55                      | 1.55                        | 1.55    | 1.55                             | 1.55                             | 1.55                             | 1.55                             | 1.55                             | 1.55                             | 1.55                             | 1.55                             |
| 1.64                   | 1.64           | 1.63                   | 1.63                   | 1.63                   | 1.63                   | 1.62                 | 2.51                                      | 1.52                       | 1.52                                                 | 1.52           | 1.52           | 1.52                           | 1.52                        | 1.52    | 1.52                   | 1.52           | 1.52                  | 1.52            | 1.52                   | 1.52                                         | 1.52                      | 1.66                 | 1.66           | 1.66                 | 1.66                 | 1.66                      | 1.66                        | 1.65    | 1.58                             | 1.58                             | 1.58                             | 1.57                             | 1.57                             | 1.57                             | 1.57                             | 1.57                             |
| -4.15                  | 4              | -3.7                   | -3.41                  | -3.35                  | -3.4                   | 0.84                 | -0.43                                     | 2.13                       | -3.74                                                | -3.8           | -4.19          | -4.25                          | -2.09                       | -4.45   | -4.4                   | -4.1           | -4.07                 | -3.35           | -3.43                  | -3.02                                        | -3.08                     | -2.54                | -2.84          | -2.3                 | -2.22                | -2.86                     | -2.3                        | -3.21   | -1.63                            | -2.29                            | -3.12                            | -4.17                            | -3.67                            | -3.35                            | -3.04                            | -0.93                            |
| 176.129                | 174.651        | 168.019                | 141.474                | 135.611                | 121.622                | 111.769              | 112.294                                   | 116.219                    | 135.663                                              | 155.099        | 175.138        | 180.210                        | 181.824                     | 187.918 | 191.161                | 185.699        | 198.606               | 205.057         | 176.308                | 188.546                                      | 175.640                   | 170.378              | 149.283        | 238.126              | 242.503              | 237.924                   | 241.940                     | 205.068 | 148.040                          | 152.131                          | 155.997                          | 174.629                          | 199.168                          | 227.940                          | 237.860                          | 242.214                          |
| 45                     | 5              | 10                     | 25                     | 40                     | 20                     | 10                   | 40                                        | 10                         | 45                                                   | 55             | 15             | 35                             | 25                          | 5       | 40                     | 55             | 20                    | 25              | 30                     | 45                                           | 25                        | 40                   | 0              | 35                   | 10                   | 25                        | 25                          | 2       | 25                               | 50                               | 50                               | 45                               | 5                                | 25                               | 35                               | 50                               |
| 2                      | 39             | -                      | 28                     | 36                     | 37                     | 46                   | 17                                        | 13                         | 39                                                   | 5              | 8              | 12                             | 49                          | 55      | 6                      | 41             | 36                    | e               | 18                     | 32                                           | 38                        | 22                   | 17             | 2                    | 30                   | 55                        | 56                          | 4       | 2                                | 2                                | 59                               | 37                               | 10                               | 56                               | 51                               | 12                               |
| 176                    | 174            | 168                    | 141                    | 135                    | 121                    | 111                  | 112                                       | 116                        | 135                                                  | 155            | 175            | 180                            | 181                         | 187     | 191                    | 185            | 198                   | 205             | 176                    | 188                                          | 175                       | 170                  | 149            | 238                  | 242                  |                           |                             |         |                                  |                                  | 155                              |                                  |                                  |                                  |                                  |                                  |
| 17.45                  | 13.81          | 10.65                  | 10                     | 13.66                  | 14 19                  | 13.87                | 13.71                                     | 16.95                      | 9.53                                                 | 7.98           | 10.68          | 14.72                          | 24.19                       | 23.28   | 24.79                  | 25.01          | 25.1                  | 14.23           | 15.39                  | 6.98                                         | 6.05                      | 5.36                 | 5.98           | 19.44                | 17.91                | 14.45                     | 11.79                       | 11.72   | 21.64                            | 20.47                            | 19.19                            | 15.65                            | 14.07                            | 15.99                            | 18.66                            | 20.4                             |
| 21 w. edge S :         | 22 w. edge S : | 23 w edge S :          | 24 w edge S :          | 25 w edge S :          | 26 w edge S            | 27 ton of culve      | 28 hottom of c                            | 29 top of phote            | 30 thalwed fro                                       | 31 thalwed     | 32 thalwed     | 33 u/s of log 1                | 34 top of phote             | -       | 36 middle of ld        | 37 S end of lo | 38 N end of lo        | 39 N end of tre | S end of tr            |                                              | 42 middle loa-            | 43 N loa-tree 1      | 44 single debr | 45 S log-tree #      | 46 N log-tree 7      | 47 Middle log-            | 48 N end of cr              |         | 50 cross secti                   | 51 cross sectiv                  | 52 cross section                 | 54 cross section                 | 55 cross section                 | 56 cross secti                   | 57 cross secti                   | 58 cross secti                   |
| 21                     | 22             | 23                     | 24                     | 25                     | 26                     | 27                   | 28                                        | 29                         | 30                                                   | 31             | 32             | 33                             | 34                          | 35      | 36                     | 37             | 38                    | 39              | 40                     | 41                                           | 42                        | 43                   | 44             | 45                   | 46                   | 47                        | 48                          | 49      | 50                               | 512                              | 53                               | 54                               | 55                               | 56                               | 57                               | 58                               |

|                                  | -       |                                          |                                          |                                          |                                               |                                             |                                             |                                             |                                             |                              |                             |               |                             |                     |         |                           |                            |                            |              |                                     |                |            |           |                              |                              |                              |                       |                                 |                                                      |                              |                              |                              |                                   |                                   |                              |                             |
|----------------------------------|---------|------------------------------------------|------------------------------------------|------------------------------------------|-----------------------------------------------|---------------------------------------------|---------------------------------------------|---------------------------------------------|---------------------------------------------|------------------------------|-----------------------------|---------------|-----------------------------|---------------------|---------|---------------------------|----------------------------|----------------------------|--------------|-------------------------------------|----------------|------------|-----------|------------------------------|------------------------------|------------------------------|-----------------------|---------------------------------|------------------------------------------------------|------------------------------|------------------------------|------------------------------|-----------------------------------|-----------------------------------|------------------------------|-----------------------------|
| -0.480 cross section from 5 to N |         | -3.806 channel bottom near bundled trees | -3.973 channel bottom near bundled trees | -3.630 channel bottom near bundled trees | -4.200 channel bottom u/s tree #4 rootwad end | -3.943 channel bottom u/s log 1 rootwad end | -4.170 channel bottom u/s log 1 rootwad end | -4.280 channel bottom u/s log 1 rootwad end | -4.286 channel bottom u/s log 1 rootwad end | -4.510 channel bottom log #5 | -4.460 channel bottom log 2 |               | -4.530 channel bottom log 2 | -4.500 N end log #5 | -4.611  | 1.884 SW edge of pavement | 1.994 S centerline of road | 2.768 N centreline of road | -            | -0.016 Backshot from BM 54 to BM 55 |                | -4.776 C/L |           | -5.126 C/L of S distributary | -5.226 C/L of S distributary | -5.396 C/L of S distributary | -5.576 C/L confluence | -5.916 confluence w/ Kitwanga K | -5.686 C/L of N distributary @ confluence of S dist. | -5.286 C/L of N distrubutary | -5.086 C/L of N distrubutary | -4.886 C/L of N distrubutary | -4.876 u/s end of dug channel C/L | -5.336 u/s end of dug channel C/L | -4.466 bole of S log-tree #7 | -4.006 DC most westerly # 1 |
|                                  |         | -8.331                                   | -7.858                                   | -8.080                                   | -14.438                                       | -13.113                                     | -16.967                                     | -16.436                                     | -15.860                                     |                              | -24.208                     |               |                             |                     | _       | -23.490                   | -22.873                    | 16.899                     | 16.328       | 0.047                               | -25.611        | -27.526    | -28.170   | -32.425                      | -37.084                      |                              |                       | -48.723                         | -41.333                                              | -32.635                      | -29.045                      | -27.071                      | -28.231                           | -39.299                           | -35.339                      | -31.256                     |
| -25.131                          | 2.735   | 0.904                                    | -0.706                                   | -2.672                                   | 0.954                                         | 2.661                                       | 0.653                                       | 0.690                                       | 0.031                                       |                              |                             |               |                             | _                   |         |                           | 26.558                     | 20.555                     | 17.068       | 0.036                               | -6.464         | -10.174    | -13.639   | -13.140                      | -16.553                      | -21.936                      | -25.623               | -27.374                         | -26.297                                              | -24.331                      | -22.407                      | -17.464                      | -15.875                           |                                   |                              | -26.231                     |
| 1.55                             | 1.55    | 1.55                                     | 1.55                                     | 1.55                                     | 1.55                                          | 1.55                                        | 1.55                                        | 1.55                                        | 1.55                                        | 1.55                         | 1.55                        | 1.55          | 1.55                        | 1.55                | 1.55    | 1.55                      | 1.55                       | 1.55                       | 1.55         | 1.36                                | 1.36           | 1.36       | 1.36      | 1.36                         | 1.36                         | 1.36                         | 1.36                  | 1.36                            | 1.36                                                 | 1.36                         | 1.36                         | 1.36                         | 1.36                              | 1.36                              | 1.36                         | 1.36                        |
| -                                | 2.16    | 2.16                                     | 2.15                                     | 2.15                                     | 2.15                                          | 2.02                                        | 2.02                                        | 2.02                                        | 2.02                                        | 1.95                         | 1.95                        | 1.95          | 1.95                        | 1.95                | 1.93    | 1.93                      | 1.93                       | 1.92                       | 1.92         | 1.6                                 | 1.6            | 1.6        | 1.6       | 1.6                          | 1.6                          | 1.6                          | 1.6                   | 1.6                             | 1.6                                                  | 1.6                          | 1.6                          | 1.6                          | 1.6                               | 1.6                               | 1.6                          | 1.6                         |
| -1.03                            | -3.1    | -3.2                                     | -3.37                                    | -3.03                                    | -3.6                                          | -3.47                                       | -3.7                                        | -3.81                                       | -3.82                                       | -4.11                        | -4.06                       | -4.09         | -4.13                       | -4.1                | -4.23   | 2.26                      | 2.37                       | 3.14                       | 3.03         | 2.57                                | -1.98          | -2.19      | -2.48     | -2.54                        | -2.64                        | -2.81                        | -2.99                 | -3.33                           | -3.1                                                 | -2.7                         | -2.5                         | -2.3                         | -2.29                             | -2.75                             | -1.88                        | -1.42                       |
| 254.819                          | 157.708 | 173.804                                  | 185.133                                  | 198.301                                  | 176.218                                       | 168.529                                     | 177.797                                     | 177.594                                     | 179.889                                     | 187.254                      | 190.369                     | 194.019       | 193.713                     | 197.776             | 190.054 | 135.454                   | 130.736                    | 50.576                     | 46.269       | 37.143                              | 99.404         | 116.138    | 135.950   | 151.079                      | 174.008                      | 193.096                      | 202.421               | 200.629                         | 205.322                                              | 215.524                      | 219.818                      | 171.661                      | 155.289                           | 192.817                           | 221.582                      | 227.622                     |
| 10                               | 30      | 15                                       | 0                                        | 2                                        | 2                                             | 45                                          | 50                                          | 40                                          | 20                                          | 15                           | 10                          | 10            | 45                          | 35                  | 15      | 15                        | 10                         | 35                         | 10           | 35                                  | 15             | 15         | 0         | 45                           | 30                           | 45                           | 15                    | 45                              | 20                                                   | 25                           | 2                            | 40                           | 20                                | 0                                 | 55                           | 20                          |
| 49                               | 42      | 48                                       | 00                                       | 18                                       | 13                                            | 31.5                                        | 47                                          | 35                                          | 53                                          | 15                           | 22                          | -             | 42                          | 46                  | e       | 27                        | 44                         | 34                         | 16           | 8                                   | 24             | 00         | 57        | 4                            | 0                            | 5                            | 25                    | 37                              | 19                                                   | 31                           | 49                           | 39                           | 17                                | 49                                | 34                           | 37                          |
| 254                              | 157     | 173                                      | 185                                      | 198                                      | 176                                           | 168                                         | 177                                         | 177                                         | 179                                         | 187                          | 190                         | 194           | 193                         | 197                 | 190     | 135                       | 130                        | 50                         | 46           | 37                                  | 66             | 116        | 135       | 151                          |                              | 193                          | 202                   | 200                             | -                                                    |                              | 1                            | -                            | 155                               |                                   |                              |                             |
| 26.04                            | 7.21    | 8.38                                     | 7 89                                     | 8.51                                     | 14 47                                         | 13 38                                       | 16.98                                       | 16.45                                       | 15.86                                       | 23.64                        | 24.61                       | 24.47         | 26.85                       | 26.48               | 26.31   | 32.96                     | 35.05                      | 26.61                      | 23.62        | 29.8                                | 11.65          | 8.67       | 621       | 96.6                         | 13.45                        | 17.56                        | 20.1                  | 26.73                           | 19.5                                                 | 10.97                        | 6.95                         | 3.4                          | 4.98                              | 15.99                             | 15.55                        | 11.2                        |
| cross secti                      | chanr   | channel ho                               | channel                                  | lannaho                                  | 64 channel ho                                 | 65 channel ho                               | 66 channel ho                               | 67 channel ho                               | 68 channel ho                               | 69 channel bo                | 70 channel bo               | 71 channel bo | 72 channel bo               | 73 N end log #      | )       | SW edge o                 | S centerline               | 77 N centrelin             | 78 W edge of | 80 Backshot fi                      | 81 C/l from lo |            | C/Latu/se | LIC/L of S dis               | C/L of S dis                 | 86 C/L of S dis              | 87 C/L conflue        | 88 confluence                   | 89 C/L of N dis                                      | 90 C/L of N dis              | 91 C/L of N dis              | 92 C/L of N di               | 93 u/s end of c                   | 94 u/s end of d                   | 95 bole of S lo              | 06 DC most w                |
| 59                               | 60      | 61                                       | 63                                       | 52                                       | 20                                            | L L L                                       | 99                                          | 67                                          | 68                                          | 69                           | 70                          | 71            | 72                          | 73                  | 74      | 75                        | 76                         | 77                         | 78           | 80                                  | 20             | 83         | 83 6      | 84                           | 85                           | 86                           | 87                    | 88                              | 80                                                   | 06                           | 6                            | 6                            | 66                                | 646                               | 96                           | OP                          |

| -30.409 | -23.447 -29.554 -4.286 DC # 2 | -22.227 -28.285 -4.256 DC # 3 | -19.731 -26.418 -4.016 DC # 4 | -16.216 -26.272 -4.116 rootwad end of N log-tree #6 | -15.989 -26.922 -4.146 rootwad end of S log-tree #7 | -9.054 -28.947 -4.526 S Bank | -12.001 -30.021 -4.916 S Bank | -13.532 -34.559 -5.136 S Bank | -18.720 -39.589 -5.216 S Bank | -25.570 -43.171 -5.536 S bank point | -28.162 -46.934 -5.676 N Bank point | -24.200 -30.410 -5.126 N Bank by DC #2 | -19.292 -26.747 -4.896 N Bank by DC #3 | -13.820 -26.020 -4.716 N Bank upstream of rootwads | -14.211 -27.357 -4.916 channel shape out from rootwads | -15.227 -28.654 -4.786 S edge of dug channel E | -19.918 -37.155 -5.146 S edge of DC W | -20.959 -36.602 -5.146 N edge of DC W | -16.340 -27.529 -4.786 N edge of DC E | -26.958 -28.755 -4.666 Photo Point 3 |
|---------|-------------------------------|-------------------------------|-------------------------------|-----------------------------------------------------|-----------------------------------------------------|------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------------|-------------------------------------|----------------------------------------|----------------------------------------|----------------------------------------------------|--------------------------------------------------------|------------------------------------------------|---------------------------------------|---------------------------------------|---------------------------------------|--------------------------------------|
| 1.36    | 1.6 1.36 -23                  | 1.6 1.36 -22                  | 1.6 1.36 -15                  | 1.6 1.36 -16                                        | 1.6 1.36 -15                                        | 1.6 1.36 -9                  | 1.6 1.36 -12                  | 1.6 1.36 -13                  | 1.6 1.36 -18                  | 1.6 1.36 -25                        | 1.6 1.36 -28                        | 1.6 1.36 -24                           | 1.36                                   | 1.6 1.36 -1                                        | 1.6 1.36 -14                                           | 1.6 1.36 -1                                    | 1.6 1.36 -19                          | 1.6 1.36 -20                          | 1.36                                  | 1.6 1.36 -2                          |
|         | -1.7                          | -1.67                         | -1.43                         | -1.53                                               |                                                     | -1.94                        | -2.33                         | -2.55                         | -2.63                         | -2.95                               |                                     | -2.54                                  |                                        |                                                    | -2.33                                                  | -2.2                                           |                                       |                                       |                                       |                                      |
| 209.364 | 223.196                       | 223.006                       | 213.199                       | 145.822                                             | 148.526                                             | 120.479                      | 136.674                       | 157.817                       | 182.750                       | 201.363                             | 203.718                             | 222.964                                | 203 706                                | 119.208                                            | 134.261                                                |                                                | 188.299                               | 193.107                               | 157.061                               | 240.713                              |
| 50      | 45                            | 20                            | 55                            | 20                                                  | 35                                                  | 45                           | 25                            | 0                             | 0                             | 45                                  | 2 12                                | 202                                    | 200                                    |                                                    |                                                        |                                                | 55                                    | 25                                    | 40                                    |                                      |
| 21      | 11                            | 0                             | 11                            |                                                     |                                                     |                              |                               | 49                            |                               |                                     |                                     |                                        |                                        |                                                    |                                                        | _                                              | -                                     | -                                     |                                       | 4                                    |
| 209     | 223                           |                               |                               |                                                     |                                                     |                              |                               |                               |                               |                                     |                                     |                                        |                                        |                                                    |                                                        |                                                |                                       |                                       | _                                     | 1.1                                  |
| 7.69    | 8.02                          | 6.26                          | 3 24                          | 1 6                                                 | 3 77                                                | 10.33                        | 8.68                          | 11.72                         | 15.9                          | 20.9                                | 75 37                               | 0.16                                   | 3 27                                   | 20.0                                               | 5 23                                                   | 240                                            | 12 50                                 | 12.24                                 | 4 15                                  | 10.32                                |


Summary of Monitoring and Evaluation at Sites 14 and 15 on the Kitwanga River

Appendix D. Fillier and Lough Letter.



March 8, 1999

BCE File: 36780-30/Kitseguecla WRP 36780-30/Kitwanga WRP Your File: Annual Agmt. 0000128 Activity 101462 Activity 12395

Bill Fell, Cedarvale Resources Ltd. WRP Coordinator Gitseguecla Band Council 36 Cascade Avenue South Hazelton, BC V0J 2R0

Dear Bill Fell:

As stated in the letter dated 02/16/99, a technical review of instream rehabilitation work in the Kitwanga and Kitseguecla Watershed Restoration Program (WRP) projects were pending draft report submissions (not received to date). We are providing these preliminary comments in lieu of the draft report submissions. The purpose of this letter is to facilitate an estimate of percentage of work completed in the Kitseguecla and Kitwanga watersheds stream rehabilitation (SR) activities for 1998/99.

Site visits to the Kitseguecla and Kitwanga stream rehabilitation activity areas were conducted on November 12, 1998. In attendance for these field visits were both Jeff Lough and Darren Fillier. We delayed our comments until draft document changes for prescription alteration approval requests, "As-Builts" with supporting documentation, and Compendium Report submissions were submitted for our review.

Both Kitseguecla and Kitwanga Standard Agreements for WRP SR activity, and respective Schedule "A"s, outlined a pertinent course of action in dealing with substantive prescription changes. Specifically, Section 4.1 of the Aquatic Habitat Rehabilitation (Works) Schedule "A" delineates that changes to the prescription, stemming from a pre-work review, were to be incorporated, in writing, into the design and then submitted to the Technical Monitor for approval. This clearly did not occur.

Ministry of Environment, Lands and Parks Environment and Lands Skeena Region Mail Address: Kispiox Forest District, Bag 5000, Smithers, BC V0J 2N0 Telephone: (250) 842-7615 Facsimile: (250) 842-7676

Location Address: 2210, Highway 62 W Hazelton BC

# Activity Number 12395 - SR - Restoration Prescription Implementation for Prescription Sites 14 and 15 Kitwanga River South Sub-Basin

Site 14 - Our first concern with this project is in regard to the pull back of the banks. This activity was not initially prescribed nor approved for work at the site. The pull back that was undertaken is of concern given its proximity to the highway and, specifically, within the road right of way. Was the Ministry of Highways consulted regarding this change?

Prescription implementation was to be as per the BioLith's 1997-98 report as delineated within the Water Act Regulations Section 9 Letter of Notification. Such prescription alteration and associated pull back to the suggested angle of repose must have been submitted for consideration by the Technical Monitor, or designate, prior to any work commencing at this site. Adherence with Section 4.1 of the Schedule "A" for Site 14 is paramount. Deviation from the prescription must follow the process as outlined within the Standard Agreement and the respective Schedule(s). Regardless of holding a Letter of Notification for specific in stream "timing windows" for work to be undertaken, the prescription alteration must be submitted for review and incorporation into a revised Letter of Notification. Clearly work should not have commenced without fulfilling all these requirements and, as such, violates Section 4.2 of the Schedule "A" and that is unacceptable to the Ministry.

Construction of the step pool system at Site 14 does not appear to be adequate to meet the goal of better facilitating fish access through the culvert. We are also concerned about the size and orientation of the materials used to construct the weirs (their long term stability is questionable). Close monitoring of this site at various flow levels, and associated modifications, will be required to fulfil the goal of creating long term fish access through the culvert.

Finally, the loss of the riparian low shrub and herb cover at Site 14 associated with the work undertaken last fall has increased surface erosion and will continue to deliver sediment into the Kitwanga River until inevitable revegitation takes place. On that note, the grass seeding that was planted seemed sporadic. In addition this surface erosion will not be mitigated by the silt fence given that its' installation was done incorrectly. This will require correction if not already done so. Again monitoring of this aspect of the project will be conducted this Spring after snowmelt.

Given the problems outlined above, no quality certificate will be issued until the site is monitored and appropriate changes are completed this Spring.

Site 15 - The Recipient provided a good source of Large Woody Debris (LWD) by species and by size. Root wad presence was good but it would be advantageous, in future, to leave branches and tops attached to the LWD pieces to increase their stability. If the objective of using rope to tie the structures together was to increase their stability, then we suggest rock anchoring would help better achieve your objective.

Sincerely,

anen J. Fillin

Darren J. Fillier, RPF, RPBio. Forest Ecosystem Specialist Kispiox Forest District

B.J.T. For

Jeff Lough WRP Fisheries Specialist Skeena Region, MELP

DJF& JL/djf & jl

attachments

cc: Doug Johnston, WRP Coordinator, Skeena Region, MELP
Dionys deLeeuw, Senior Habitat Protection Biologist, Skeena Region, MELP
Brian Fuhr, Habitat Protection Section Head, Skeena Region, MELP
Bob Purdon, Skeena-Bulkley Region, Forest Renewal BC
Bert Mast, Skeena-Bulkley Region, Forest Renewal BC
Eero Karanka, Habitat Biologist, Department of Fisheries and Oceans, Smithers, BC
Darlene Morgan, Gitsegukla Band Council

Summary of Monitoring and Evaluation at Sites 14 and 15 on the Kitwanga River

Appendix E. Harkleroad Letter.

Pairen FILLIER Pacil Nov 12/98

## British Columbia Stream Restoration Project Review Report 1998

#### USFS Contact: Glenn R. Harkleroad, Fisheries Biologist

BC Contact: Jeff Lough, Fisheries Specialist

This report will be divided into two parts. The first part will be a review of the projects Jeff and I, as well as other Ministry personnel, reviewed while I was visiting in British Columbia the week of September 21 - 25, 1998. The second part of this report will be an overview of potential monitoring activities that could be used to evaluate instream restoration activities.

Photos of sites that were reviewed in the field have been forwarded to Jeff Lough.

### **Project Reviews**

#### River System: Kitwonga Stream system: Tea Creek

Site review by: Jeff Lough, Darren Fillier, and Glenn Harkleroad

Project Background: This project consisted of 10 to 12 channel spanning weirs created by cement "lock-blocks" below a 1.5 meter culvert. The "lock-blocks" were placed to raise the level of the streambed with the intent of helping pass fish through the upstream highway culvert. The "lock-blocks" had been placed and re-enforced by rock riprap ranging in size from 15 to 60 cm. The "lock-block" weirs were placed approximately 4 to 5 meters apart and were placed perpendicular to the stream channel. The local highway authority had completed this work.

Stream Conditions: The stream passed through a 1.5 meter culvert below highway 16. The structures began immediately below the culvert and continued down stream approximately 30 meter. The stream was bordered on the right by a small access road. When this road was constructed the road cut/base material had been sidecast into the floodprone and bankfull stream channel. Most of the immediate stream side vegetation in the local area had been removed during highway and access road construction. Some vegetative recovery had occurred.

Restoration Design Concerns: While reviewing this site a number of project design concerns surfaced. These concerns included the following:

- "Lock-block" weirs appeared to be placed too close together. The plunge created by the upstream weirs may have a scouring effect on weirs immediately downstream resulting in design failure.
- 2) The perpendicular placement of the weirs may result in channel widening, thereby increasing the localized channel width to depth ratio. This may eventually result in bank erosion and "end cutting" around the weir structures.

One other item that was discussed at this site was the alteration of road design to reduce channel diversion potential associated with culvert plugging. As the road is currently designed, if the culvert plugs, water will be diverted out the left side of the channel, down the road and will eventually cross the road approximately 25 meters from the stream channel (Figure 1). This would result in the loss of road fill and the potential to deliver road fill associated sediment to Tea Creek. Altering the road grade in the vicinity of the culvert could mitigate this concern. The creation of a dip above the culvert, would allow water and debris to pass over the road and directly back onto Tea Creek in the event the culvert became plugged. This would minimize potential sediment delivery to Tea Creek as well as reduce road repair cost since only the fill immediately above the culvert would have the potential to be lost. If this fill was made of primarily of large rock with a driving surface cap, fine sediment delivery and repair cost could be kept to a minimum.

# River System: Kitwonga Stream system: un-named tributary #1 (Kitwonga) Pres. Site # 15.)

Site review by: Jeff Lough, Darren Fillier, and Glenn Harkleroad

Project Background: This project site was an approximate 90 to 100 meter length of stream below a highway culvert that fed directly into the Kitwonga River. This area had been identified for large wood placement in order to improve juvenile salmonid rearing habitat. This relatively small project would also serve as a trial run project for a new contractor.

The proposed wood placement locations had been flagged and consisted primarily of placing single logs in more or less and alternating pattern down the length of the channel. The logs would be anchored to streamside trees with cable. Boulders and rootwads currently present within the stream would also be used to help stabilize the placed wood.

Project Comments: While in the field at this site we talked about a number of different design options. The first of these options was to consider experimenting with log anchoring techniques. The option of cable anchoring some logs, while just using channel features and streamside trees to stabilize other logs was discussed. If this is done during the project implementation, this project could serve as an area to compare the effectiveness of both techniques.

We also discussed specific project designs for the lower 20 to 25 meters of the stream channel. Figure 2 displays the project design that was discussed for this location in the field. The idea was to direct the water toward the right side of the channel with the idea of reducing the bank cutting / mass wasting which was occurring along the left bank. There would be some bank cutting expected along the right bank, but it would be expected to be fairly minor and well within the range of natural channel adjustment. The placement of a log complex along the left bank was recommended to further discourage cutting along this bank. The use of log complexes, instead of just single logs, was suggested to more closely mimic natural wood accumulation within the channel.

Recommendations: While at this site, we also discussed some potential monitoring items. These included photo points, topographic surveys of the channel, and sketching desired post-project channel conditions. Since this project would be completed by a relatively inexperienced contractor, I would recommend having him take photo points and having him sketch what he envisions the post-project channel will look like.

#### River System: Kitwonga

Stream system: un-named tributary #2 Kitwangin Pies. Site #14

Site review by: Jeff Lough, Darren Fillier, and Glenn Harkleroad

Project Background: This project was similar to the project proposed for un-named tributary #1 in that it was an approximate 30 to 35 meter length of stream below a highway culvert which fed directly into the Kitwonga River. This area had been identified for large wood placement in order to improve juvenile salmonid rearing habitat. This relatively small project would also serve as a trial run project for a new contractor. However the stream channel in this area was much higher gradient and lacked the channel diversity seen in the first tributary.

This project also involved trying to create a series of step pools for trying to raise the streambed, in order to pass fish through the highway culvert. Channel conditions and available habitat above the culvert were unknown.

Project Comments: The stream channel below the culvert was relatively steep and appeared to provide little fish habitat. Placing wood in this channel would be expected to have low chance of success for meeting the goal of increasing fish habitat. This is because the natural condition of this channel does not lend itself to providing good spawning or rearing habitat.

Passage at the culvert should be delayed until fish habitat values above the culvert are determined. Without this information, it is possible that time and money could be spent providing fish access to an area with very little habitat value.

Recommendations: I would recommend determining if there are other higher priority areas where work could be done. Initial field review of this project would suggest that it would be low priority.

#### River System: Kispiox

Stream system: un-named tributary #1 (Dale cle).

Site review by: Jeff Lough, Darren Fillier, and Glenn Harkleroad

Project Background: This project consisted of two rows of "lock blocks" which were placed in a small tributary of the Kispiox River with the intent of raising the streambed level below two culverts. This was done in order to help facilitate fish passage through the culverts. We were reviewing this project because the design used was not authorized by Ministry fisheries personnel and was going to be changed.

The "lock block" weirs were placed approximately 6 to 7 meters apart and were arranged perpendicular to the stream flow. There were concerns that this design would increase the stream channel width to depth ratio and result in end cutting around the weirs. Excessive fine sediment deposition had already begun above the upper weir. This was resulting in the filling of the jump pool necessary for fish passage through the culverts. There was also a concern that the weirs were too placed close together and that the scour created by the upper weir would undermine the lower one.

While reviewing the project we also discovered that the inlets of both culverts were blocked by a log that had backed up sediment. making fish passage difficult during most flows ...

Summary of Monitoring and Evaluation at Sites 14 and 15 on the Kitwanga River

Appendix F. Centreline Survey, March, 1999.





